

- Abnormal Over-Current Protection (AOCP)
- Auto-Restart Mode
- Under-Voltage Lock Out (UVLO) with Hysteresis
- Low Operating Current: 2.5mA
- Built-in Soft-Start

# Applications

- SMPS for LCD Monitor and STB
- Adaptor

### Description

The FSDM0465RS is an integrated Pulse-Width Modulator (PWM) and SenseFET specifically designed for high-performance offline Switch Mode Power Supplies (SMPS) with minimal external components. The device is an integrated, high-voltage, powerswitching regulator that combines an avalanche rugged SenseFET with a current mode PWM control block. The PWM controller includes integrated fixed-frequency oscillator, under-voltage lockout, leading-edge blanking (LEB), optimized gate driver, internal soft-start, temperature-compensated precise-current sources for a loop compensation and self-protection circuitry. Compared with a discrete MOSFET and PWM controller solution, it reduces total cost, component count, size and weight; while increasing efficiency, productivity and system reliability. This device is a basic platform well suited for cost effective designs of flyback converters.

## **Ordering Information**

Product Number	Package	Eco Status	Marking Code	BV <sub>DSS</sub>	R <sub>DS(ON)</sub> Max.
FSDM0465RSWDTU <sup>(1)</sup>	TO-220F-6L(Forming)	RoHS	DM0465RS	650V	2.6Ω

Note:

1. WDTU: Forming Type.

For Fairchild's definition of "green" Eco Status, please visit: <u>http://www.fairchildsemi.com/company/green/rohs\_green.html</u>.

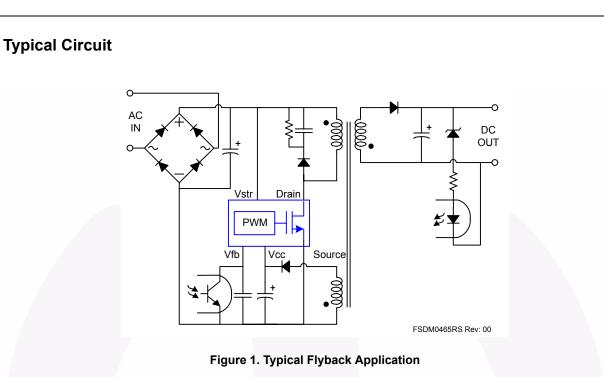
FPS<sup>™</sup> is a trademark of Fairchild Semiconductor Corporation.

#### April 2009

FAIRCHILD SEMICONDUCTOR

FSDM0465RS

Features

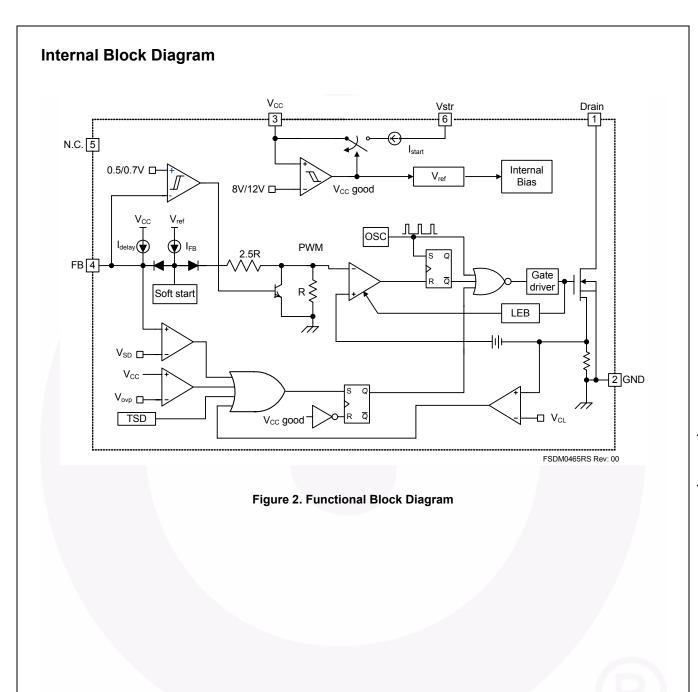




		Maximum Ou	tput Power <sup>(2)</sup>	
Product	230V <sub>AC</sub> ±15% <sup>(3)</sup>		85-20	65V <sub>AC</sub>
	Adapter <sup>(4)</sup>	Open Frame <sup>(5)</sup>	Adapter <sup>(4)</sup>	Open Frame <sup>(5)</sup>
FSDM0465RS	48W	56W	40W	48W

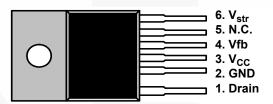
#### Notes:

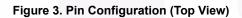
- The junction temperature can limit the maximum output power.  $230V_{AC}$  or  $100/115V_{AC}$  with doubler. 2.
- 3.
- 4. Typical continuous power in a non-ventilated enclosed adapter measured at 50°C ambient temperature.
- 5. Maximum practical continuous power in an open-frame design at 50°C ambient.



# **Pin Configuration**







# **Pin Definitions**

Pin #	Name	Description			
1	Drain	SenseFET drain. High-voltage power SenseFET drain connection.			
2	GND	Ground. This pin is the control ground and the SenseFET source.			
3	V <sub>CC</sub>	<b>Power Supply</b> . This pin is the positive supply input, providing internal operating current for both startup and steady-state operation.			
4	Vfb	<b>Feedback</b> . This pin is internally connected to the inverting input of the PWM comparator. The collector of an opto-coupler is typically tied to this pin. For stable operation, a capacitor should be placed between this pin and GND. If the voltage of this pin reaches 6V, the overload protection triggers, which shuts down the FPS.			
5	N.C.	No Connection.			
6	V <sub>str</sub>	<b>Startup</b> . This pin is connected directly, or through a resistor, to the high-voltage DC link. At startup, the internal high-voltage current source supplies internal bias and charges the external capacitor connected to the $V_{CC}$ pin. Once $V_{CC}$ reaches 12V, the internal current source is disabled. It is not recommended to connect $V_{str}$ and Drain together.			

# **Absolute Maximum Ratings**

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.  $T_A = 25^{\circ}C$ , unless otherwise specified.

Symbol	Parameter		Value	Unit
BV <sub>DSS</sub>	Drain Source Breakdown Voltage		650	V
V <sub>STR</sub>	V <sub>STR</sub> Maximum Voltage		650	V
I <sub>DM</sub>	Drain Current Pulsed <sup>(6)</sup>	T <sub>C</sub> =25°C	9.6	A <sub>DC</sub>
1-	Continuous Drain Current <sup>(7)</sup>	T <sub>C</sub> =25°C	2.2	A <sub>RMS</sub>
Ι <sub>D</sub>		T <sub>C</sub> =100°C	1.4	A <sub>RMS</sub>
E <sub>AS</sub>	Single Pulsed Avalanche Energy <sup>(8)</sup>		120	mJ
V <sub>CC</sub>	Supply Voltage		20	V
V <sub>FB</sub>	Input Voltage Range		-0.3 to 12	V
P <sub>D</sub> (Watt H/S)	Total Power Dissipation (Tc=25°C)		45	W
Τ <sub>J</sub>	Operating Junction Temperature		Internally limited	°C
T <sub>A</sub>	Operating Ambient Temperature		-25 to +85	°C
T <sub>STG</sub>	Storage Temperature		-55 to +150	°C
ESD	ESD Capability, Human Body Model, JESD22-A114 (All pins excepts for $\rm V_{STR}$ and $\rm V_{FB})$		2.0 (GND-V <sub>STR</sub> /V <sub>FB</sub> =1.5kV)	kV
LOD	ESD Capability, Charged Device Model, JESD22-C101		1.0	kV

Notes:

6. Repetitive rating: pulse width limited by maximum junction temperature.

7. This value is RMS current rating which should not be confused by the switching current.

8. L=14mH, starting  $T_J$ =25°C.

# **Thermal Impedance**

T<sub>A</sub>=25°C, unless otherwise specified.

Symbol	Parameter	Value	Unit
$\theta_{JA}^{(9)}$	Junction-to-Ambient Thermal	50	°C/W
$\theta_{JC}^{(10)}$	Junction-to-Case Thermal	2.78	°C/W

#### Notes:

9. Free standing with no heat-sink under natural convection.

10. Infinite cooling condition - Refer to the SEMI G30-88.

# **Electrical Characteristics**

 $T_A = 25^{\circ}C$  unless otherwise specified.

Symbol	Parameter	Condition	Min.	Тур.	Max.	Unit
SenseFET	SECTION			•		
		V <sub>DS</sub> = 650V, V <sub>GS</sub> = 0V			250	μA
I <sub>DSS</sub>	Zero Gate Voltage Drain Current	$V_{DS}$ = 520V, $V_{GS}$ = 0V, T <sub>C</sub> = 125°C			250	μA
R <sub>DS(ON)</sub>	Static Drain Source on Resistance <sup>(11)</sup>	V <sub>GS</sub> = 10V, I <sub>D</sub> = 2.5A		2.2	2.6	Ω
C <sub>OSS</sub>	Output Capacitance	V <sub>GS</sub> = 0V, V <sub>DS</sub> = 25V, f = 1MHz		60		pF
t <sub>d(on)</sub>	Turn-On Delay Time			23		
t <sub>r</sub>	Rise Time			20		ns
t <sub>d(off)</sub>	Turn-Off Delay Time	– V <sub>DD</sub> = 325V, I <sub>D</sub> = 5A		65		
t <sub>f</sub>	Fall Time			27		
CONTROL	SECTION					
f <sub>OSC</sub>	Switching Frequency	V <sub>FB</sub> = 3V	60	66	72	kHz
$\Delta f_{STABLE}$	Switching Frequency Stability	$13V \le V_{CC} \le 18V$	0	1	3	%
$\Delta f_{OSC}$	Switching Frequency Variation <sup>(12)</sup>	$-25^{\circ}C \leq T_A \leq 85^{\circ}C$	0	±5	±10	%
I <sub>FB</sub>	Feedback Source Current	V <sub>FB</sub> = GND	0.7	0.9	1.1	mA
D <sub>MAX</sub>	Maximum Duty Cycle		77	82	87	%
D <sub>MIN</sub>	Minimum Duty Cycle				0	%
V <sub>START</sub>		V <sub>FB</sub> = GND	11	12	13	V
V <sub>STOP</sub>	UVLO Threshold Voltage	V <sub>FB</sub> = GND	7	8	9	V
t <sub>S/S</sub>	Internal Soft-Start Time	V <sub>FB</sub> = 3V		10	15	ms
BURST MO	ODE SECTION			•	•	
V <sub>BURH</sub>	Durat Made Valtages	V <sub>CC</sub> = 14V		0.7		V
V <sub>BURL</sub>	Burst Mode Voltages	V <sub>CC</sub> = 14V		0.5		V
	ION SECTION					
V <sub>SD</sub>	Shutdown Feedback Voltage	$V_{FB} \ge 5.5V$	5.5	6.0	6.5	V
IDELAY	Shutdown Delay Current	V <sub>FB</sub> = 5V	2.8	3.5	4.2	μA
t <sub>LEB</sub>	Leading Edge Blanking Time <sup>(12)</sup>			250		ns
I <sub>LIMIT</sub>	Peak Current Limit <sup>(13)</sup>	V <sub>FB</sub> = 5V, V <sub>CC</sub> = 14V	1.6	1.8	2.0	А
V <sub>OVP</sub>	Over-Voltage Protection		18	19	20	V
T <sub>SD</sub>	Thermal Shutdown Temperature <sup>(12)</sup>		+130	+145	+160	°C
TOTAL DE	VICE SECTION					
I <sub>START</sub>	Operating Supply Current <sup>(14)</sup>	V <sub>FB</sub> = GND, V <sub>CC</sub> = 11V		1.0	1.3	mA
I <sub>OP</sub>		$V_{FB} = GND, V_{CC} = 14V$				
I <sub>OP(MIN)</sub>	Operating Supply Current <sup>(14)</sup>	$V_{FB} = GND, V_{CC} = 10V$	1	2.5	5.0	mA
		$V_{FB} = GND, V_{CC} = 18V$		1	I	1

### Notes:

11. Pulse test: Pulse width  $\leq 300 \mu S, \, duty \leq 2\%.$ 

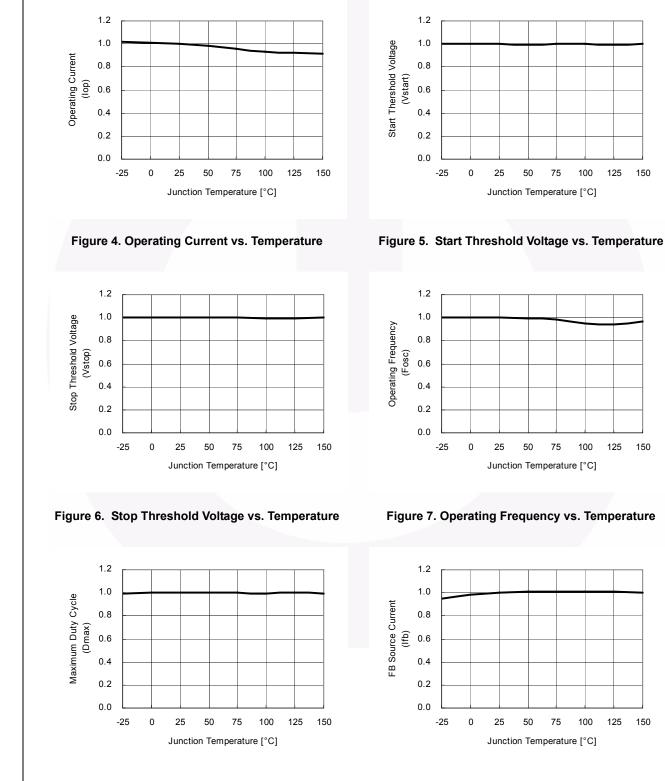
12. These parameters, although guaranteed at the design, are not tested in mass production.

13. These parameters indicate the inductor current.

14. This parameter is the current flowing into the control IC.

# Comparison Between FS6M07652RTC and FSDM0465RS

Function	FS6M07652RTC	FSDM0465RS	FSDM0465RS Advantages
Soft-Start	Adjustable soft-start time using an external capacitor	Internal soft-start with typically 10ms (fixed)	<ul> <li>Gradually increasing current limit during soft-start further reduces peak current and voltage component stresses</li> <li>Eliminates external components used for soft-start in most applications</li> <li>Reduces or eliminates output overshoot</li> </ul>
Burst Mode Operation	<ul> <li>Built into controller</li> <li>Output voltage drops to around half</li> </ul>	<ul><li>Built into controller</li><li>Output voltage fixed</li></ul>	<ul> <li>Improve light-load efficiency</li> <li>Reduces no-load consumption</li> </ul>





**Typical Performance Characteristics** 

Graphs are normalized at  $T_A$ = 25°C.

Figure 9. Feedback Source Current vs. Temperature

125

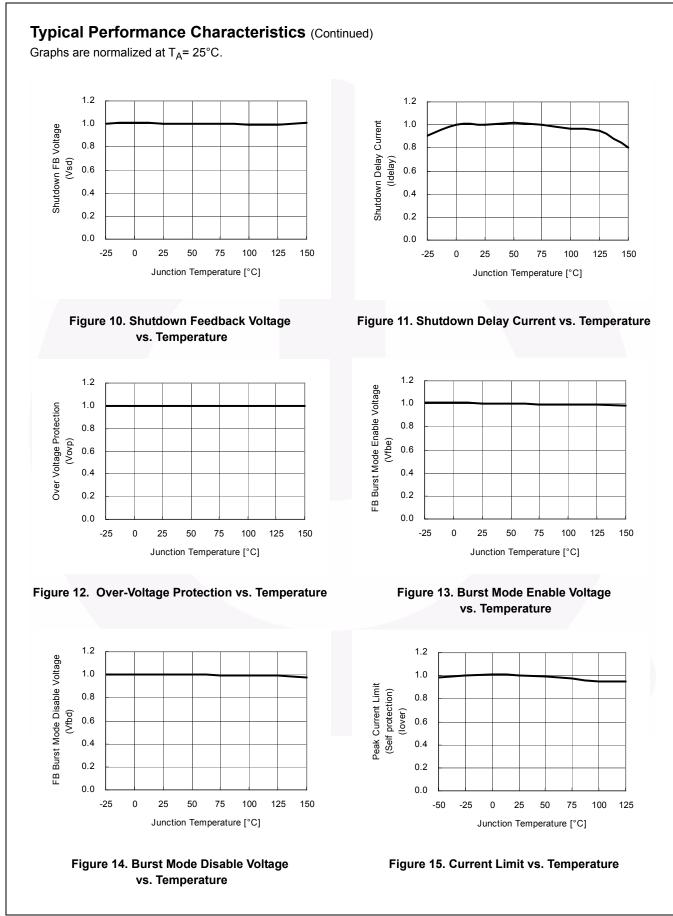
125

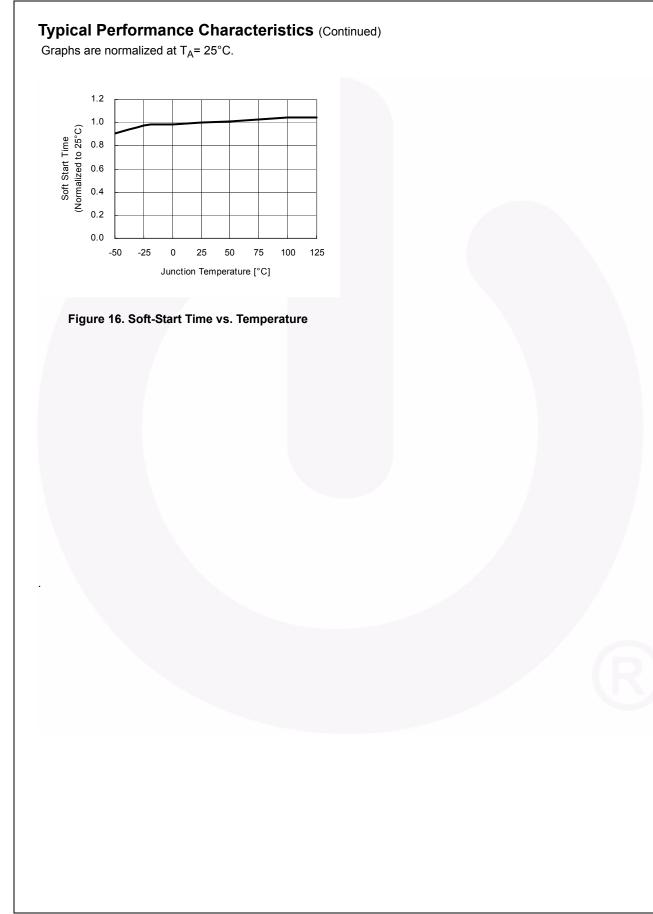
125

150

150

150





## **Functional Description**

**1. Startup**: In previous generations of Fairchild Power Switches (FPS<sup>TM</sup>) the V<sub>CC</sub> pin had an external startup resistor to the DC input voltage line. In this generation the startup resistor is replaced by an internal high-voltage current source. At startup, an internal high-voltage current source supplies the internal bias and charges the external capacitor (C<sub>vcc</sub>) that is connected to the V<sub>CC</sub> pin shown in Figure 17. When V<sub>CC</sub> reaches 12V, the FSDM0465RS begins switching and the internal high-voltage current source is disabled. The FSDM0465RS continues its normal switching operation and the power is supplied from the auxiliary transformer winding unless V<sub>CC</sub> goes below the stop voltage of 8V.

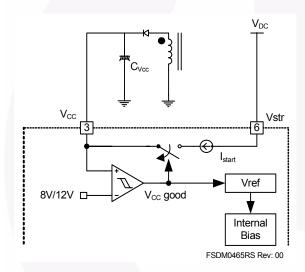


Figure 17. Internal Startup Circuit

2. Feedback Control: FSDM0465RS employs current mode control, as shown in Figure 18. An opto-coupler (such as the H11A817A) and shunt regulator (such as the KA431) are typically used to implement the feedback network. Comparing the feedback voltage with the voltage across the  $R_{SENSE}$  resistor plus an offset voltage makes it possible to control the switching duty cycle. When the reference pin voltage of the KA431 exceeds the internal reference voltage of 2.5V, the H11A817A LED current increases, thus pulling down the feedback voltage and reducing the duty cycle. This event typically happens when the input voltage is increased or the output load is decreased.

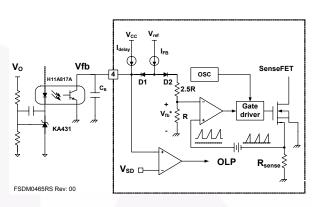
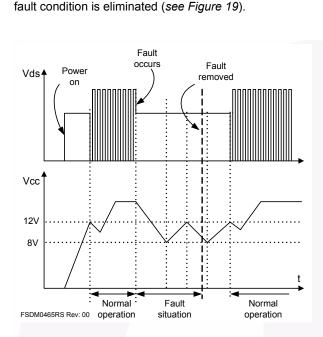


Figure 18. Pulse Width Modulation (PWM) Circuit

**2.1 Pulse-by-Pulse Current Limit**: Because current mode control is employed, the peak current through the SenseFET is limited by the inverting input of PWM comparator ( $V_{FB}^*$ ) as shown in Figure 18. Assuming that the 0.9mA current source flows only through the internal resistor (2.5R + R = 2.8k $\Omega$ ), the cathode voltage of diode D2 is about 2.5V. Since D1 is blocked when the feedback voltage ( $V_{FB}$ ) exceeds 2.5V, the maximum voltage of the cathode of D2 is clamped at this voltage, thus clamping  $V_{FB}^*$ . Therefore, the peak value of the current through the SenseFET is limited.

**2.2 Leading-Edge Blanking (LEB)**: At the instant the internal SenseFET is turned on, there usually exists a high-current spike through the SenseFET, caused by primary-side capacitance and secondary-side rectifier reverse recovery. Excessive voltage across the R<sub>SENSE</sub> resistor would lead to incorrect feedback operation in the current mode PWM control. To counter this effect, the FSDM0465RS employs a leading edge blanking (LEB) circuit. This circuit inhibits the PWM comparator for a short time ( $t_{LEB}$ ) after the SenseFET is turned on.

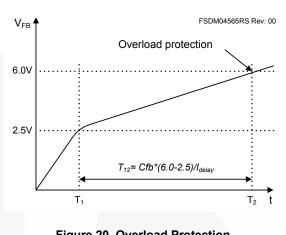
**3. Protection Circuit**: The FSDM0465RS has several self protective functions such as overload protection (OLP), over-voltage protection (OVP) and thermal shutdown (TSD). Because these protection circuits are fully integrated into the IC without external components, the reliability is improved without increasing cost. Once the fault condition occurs, switching is terminated and the SenseFET remains off. This causes  $V_{CC}$  to fall. When  $V_{CC}$  reaches the UVLO stop voltage, 8V, the protection is reset and the internal high-voltage current source charges the  $V_{CC}$  capacitor via the Vstr pin. When  $V_{CC}$  reaches the UVLO start voltage, 12V, the FSDM0465RS resumes its normal operation. In this manner, the auto-restart can alternately enable and



disable the switching of the power SenseFET until the

Figure 19. Auto Restart Operation

3.1 Overload Protection (OLP): Overload is defined as the load current exceeding a pre-set level due to an unexpected event. In this situation, the protection circuit should be activated to protect the SMPS. However, even when the SMPS is in the normal operation, the overload protection circuit can be activated during the load transition. To avoid this undesired operation, the overload protection circuit is designed to be activated after a specified time to determine whether it is a transient situation or an overload situation. Because of the pulse-by-pulse current limit capability, the maximum peak current through the SenseFET is limited, and therefore the maximum input power is restricted with a given input voltage. If the output consumes beyond this maximum power, the output voltage (V<sub>O</sub>) decreases below the set voltage. This reduces the current through the opto-coupler LED, which reduces the opto-coupler transistor current, thus increasing the feedback voltage  $(V_{FB})$ . If  $V_{FB}$  exceeds 2.5V, D1 is blocked and the 3.5µA current source starts to charge  $C_B$  slowly up to  $V_{CC}.$  In this condition, V<sub>FB</sub> continues increasing until it reaches 6V, when the switching operation is terminated as shown in Figure 20. The delay time for shutdown is the time required to charge  $C_B$  from 2.5V to 6.0V with 3.5µA. In general, a 10 ~ 50ms delay time is typical for most applications.



**Figure 20. Overload Protection** 

3.2 Over-Voltage Protection (OVP): If the secondary side feedback circuit were to malfunction or a solder defect caused an open in the feedback path, the current through the opto-coupler transistor becomes almost zero. Then, V<sub>FB</sub> climbs up in a similar manner to the overload situation, forcing the preset maximum current to be supplied to the SMPS until the overload protection is activated. Because more energy than required is provided to the output, the output voltage may exceed the rated voltage before the overload protection is activated, resulting in the breakdown of the devices in the secondary side. To prevent this situation, an overvoltage protection (OVP) circuit is employed. In general, V<sub>CC</sub> is proportional to the output voltage and the FSDM0465RS uses V<sub>CC</sub> instead of directly monitoring the output voltage. If V<sub>CC</sub> exceeds 19V, an OVP circuit is activated resulting in the termination of the switching operation. To avoid undesired activation of OVP during normal operation, V<sub>CC</sub> should be designed to be below 19V.

3.3 Thermal Shutdown (TSD): The SenseFET and the control IC are built in one package. This makes it easy for the control IC to detect the heat generation from the SenseFET. When the temperature exceeds approximately 150°C, the thermal shutdown is activated.

4.2 Abnormal Over-Current Protection (AOCP): When the secondary rectifier diodes or the transformer pins are shorted, a steep current with extremely high di/dt can flow through the SenseFET during the LEB time. Even though the FPS has overload protection, it is not enough to protect the FPS in those abnormal cases, since severe current stress is imposed on the SenseFET until OLP triggers. This IC has an internal AOCP circuit shown in Figure 21. When the gate turn-on signal is applied to the power SenseFET, the AOCP block is enabled and monitors the current through the sensing resistor. The voltage across the resistor is compared with a preset AOCP level. If the sensing resistor voltage is

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greater than the AOCP level, the set signal is applied to the latch, resulting in the shutdown of the SMPS.

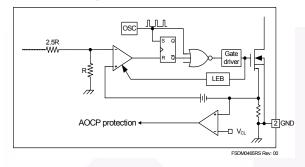


Figure 21. Abnormal Over-Current Protection

**4. Soft-Start**: The FSDM0465RS has an internal softstart circuit that increases PWM comparator inverting input voltage together with the SenseFET current slowly after it starts up. The typical soft-start time is 10ms. The pulse width to the power switching device is progressively increased to establish the correct working conditions for transformers, inductors, and capacitors. The voltage on the output capacitors is progressively increased with the intention of smoothly establishing the required output voltage. It helps prevent transformer saturation and reduces the stress on the secondary diode during startup.

**5.** Burst Operation: To minimize power dissipation in standby mode, the FSDM0465RS enters burst mode operation. As the load decreases, the feedback voltage decreases. As shown in Figure 22, the device automatically enters burst mode when the feedback voltage drops below  $V_{BURL}(500\text{mV})$ . At this point switching stops and the output voltages start to drop at a rate dependent on standby current load. This causes the feedback voltage to rise. Once it passes  $V_{BURH}(700\text{mV})$  switching resumes. The feedback voltage then falls and the process repeats. Burst mode operation alternately enables and disables switching of the power SenseFET thereby reducing switching loss in standby mode.

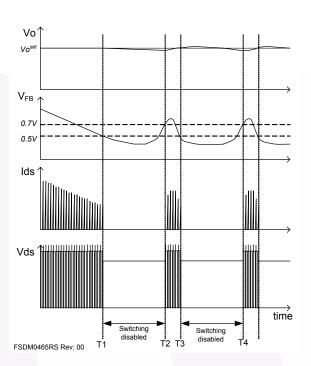


Figure 22. Waveforms of Burst Operation

# **Typical Application Circuit**

Application	Output Power	Input Voltage	Output Voltage (Maximum Current)
LCD Monitor	34W	Universal Input (85-265V <sub>AC</sub> )	5V (2.0A) 12V (2.0A)

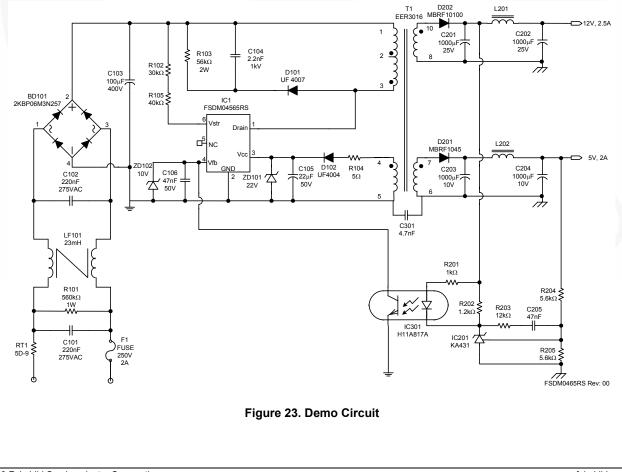
### Features

- High Efficiency (>81% at 85V<sub>AC</sub> Input)
- Low Zero Load Power Consumption (<300mW at 240V<sub>AC</sub> Input)
- Low Standby Mode Power Consumption (<800mW at 240V<sub>AC</sub> Input and 0.3W Load)
- Low Component Count
- Enhanced System Reliability through Various Protection Functions
- Internal Soft-Start (10ms)

### **Key Design Notes**

- Resistors R102 and R105 are employed to prevent startup at low input voltage. After startup, there is no power loss in these resistors since the startup pin is internally disconnected after startup.
- The delay time for overload protection is designed to be about 50ms with C106 of 47nF. If a faster triggering of OLP is required, C106 can be reduced to 10nF.
- Zener diode ZD102 is used for a safety test such as UL. When the drain pin and feedback pin are shorted, the zener diode fails and remains short, which causes the fuse (F1) blown and prevents explosion of the opto-coupler (IC301). This zener diode also increases the immunity against line surge.

#### 1. Schematic



### 2. Transformer

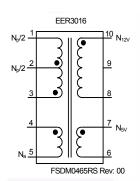


Figure 24. Transformer Schematic Diagram

### **3.Winding Specification**

No	Pin (s→f)	Wire	Turns	Winding Method
Na	$4 \rightarrow 5$	$0.2^{\varphi}  imes 1$	8	Center Winding
Insulation: F	Polyester Tape t = 0.050	mm, 2 Layers		
Np/2	$2 \rightarrow 1$	$0.4^{\phi}  imes 1$	18	Solenoid Winding
Insulation: F	Polyester Tape t = 0.050	mm, 2 Layers		
N <sub>12V</sub>	$10 \rightarrow 8$	$0.3^{\phi}  imes 3$	7	Center Winding
Insulation: F	Polyester Tape t = 0.050	mm, 2 Layers		
N5V	$7 \rightarrow 6$	$0.3^{\varphi}\times 3$	3	Center Winding
Insulation: F	Polyester Tape t = 0.050	mm, 2 Layers	· · ·	
Np/2	$3 \rightarrow 2$	$0.4^{\varphi}  imes 1$	18	Solenoid Winding
Outer Insula	ation: Polyester Tape t =	0.050mm, 2 Layers		

### **4.Electrical Characteristics**

	Pin	Specification	Remarks
Inductance	1 - 3	650µH ± 10%	100kHz, 1V
Leakage Inductance	1 - 3	10µH Maximum	2 <sup>nd</sup> all short

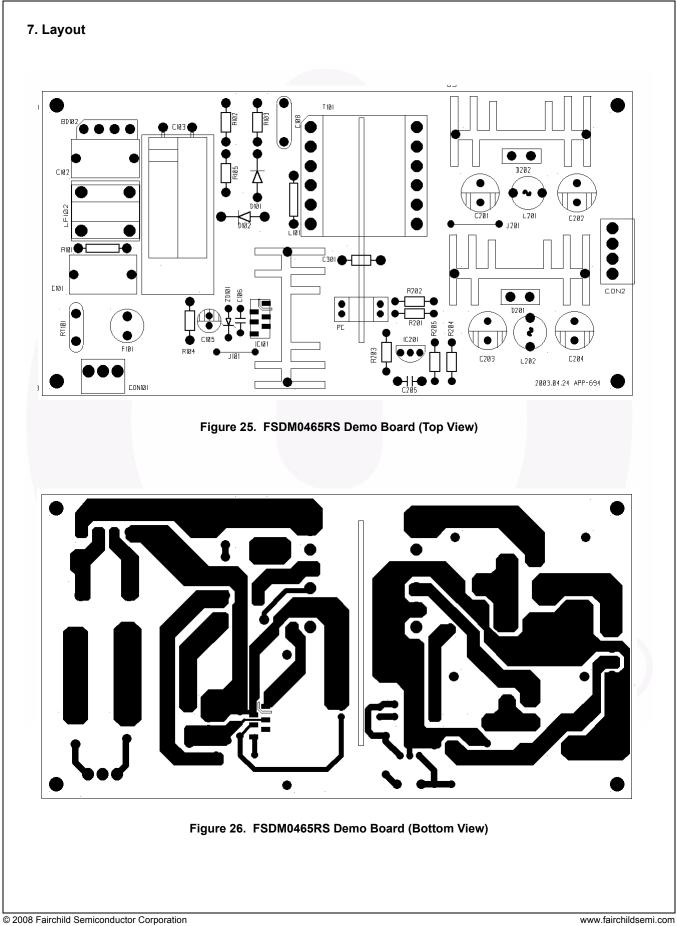
### 5. Core & Bobbin

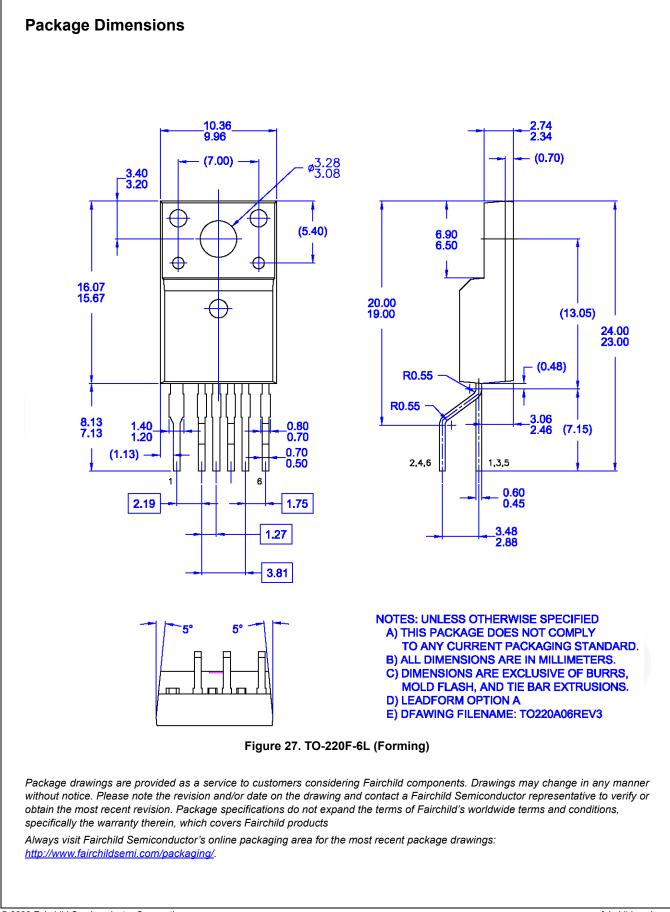
- Core: EER 3016
- Bobbin: EER3016
- Ae(mm2): 96

FSDM0465RS — Green Mode Fairchild Power Switch (FPS™)

### 6. Demo Circuit Part List

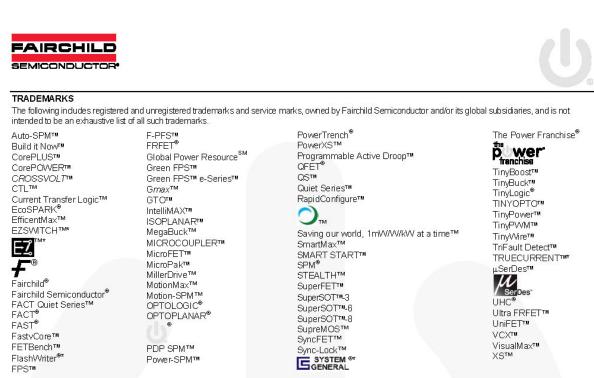
Part	Value	Note	Part	Value	Note
	Fu	se		Induc	tor
F101	2A/250V		L201	5µH	Wire 1.2mm
	NT	C	L202	5µH	Wire 1.2mm
RT101	5D-9			Dioc	le
	Resi	stor	D101	UF4007	
R101	560kΩ	1W	D102	UF4004	
R102	<b>30k</b> Ω	1/4W	D201	MBRF1045	
R103	56kΩ	2W	D202	MBRF10100	
R104	5Ω	1/4W	ZD101	Zener Diode	22V
R105	40kΩ	1/4W	ZD102	Zener Diode	10V
R201	1kΩ	1/4W		Bridge	Diode
R202	1.2kΩ	1/4W	BD101	2KBP06M 3N257	Bridge Diode
R203	12kΩ	1/4W			
R204	5.6kΩ	1/4W		Line Filter	
R205	5.6kΩ	1/4W	LF101	23mH	Wire 0.4mm
				IC	
	Сара	citor	IC101	FSDM0465RS	FPS™
C101	220nF/275V <sub>AC</sub>	Box Capacitor	IC201	KA431 (TL431)	Voltage Reference
C102	220nF/275V <sub>AC</sub>	Box Capacitor	IC301	H11A817A	Opto-coupler
C103	100µF/400V	Electrolytic Capacitor			
C104	2.2nF/1kV	Ceramic Capacitor			
C105	22uF/50V	Electrolytic Capacitor			
C106	47nF/50V	Ceramic Capacitor			
C201	1000µF/25V	Electrolytic Capacitor			
C202	1000µF/25V	Electrolytic Capacitor			
C203	1000µF/10V	Electrolytic Capacitor			
C204	1000µF/10V	Electrolytic Capacitor			
C205	47nF/50V	Ceramic Capacitor			
C301	4.7nF	Polyester Film Capacitor			





FSDM0465RS

Green Mode Fairchild Power Switch (FPS™)



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Preliminary	First Production	Datasheet contains preliminary data, supplementary data will be published at a later date. Fairchild Semiconductor reserves the right to make changes at any time without notice to improve design.			
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